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## Structure Reports

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## Diethylenetriaminium hexafluorido-titanate(IV) fluoride

J. Lhoste, K. Adil,\* M. Leblanc and V. Maisonneuve

Laboratoire des Oxydes et Fluorures, UMR 6010 CNRS, Faculté des Sciences et Techniques, Université du Maine, Avenue Olivier Messiaen, 72085 Le Mans Cedex 9, France

Correspondence e-mail: karim.adil@univ-lemans.fr

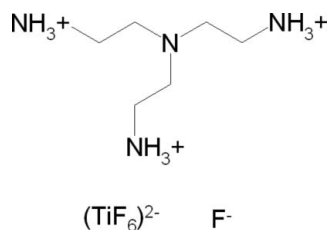
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Key indicators: single-crystal X-ray study;  $T = 298$  K; mean  $\sigma(\text{C}-\text{C}) = 0.007$  Å;  $R$  factor = 0.0611;  $wR$  factor = 0.155; data-to-parameter ratio = 18.5.

The title compound,  $(\text{C}_6\text{H}_{21}\text{N}_4)[\text{TiF}_6]\text{F}$ , was synthesized by the reaction of  $\text{TiO}_2$ , tris(2-aminoethyl)amine, HF and ethanol at 463 K in a microwave oven. The crystal structure consists of two crystallographically independent  $[\text{TiF}_6]^{2-}$  anions, two fluoride anions and two triply-protonated tris(2-aminoethyl)-amine cations. The Ti atoms are coordinated by six F atoms within slightly distorted octahedra. The anions and cations are connected by intermolecular  $\text{N}-\text{H}\cdots\text{F}$  hydrogen bonds.

## Related literature

For background, see: Adil *et al.* (2006). For related structures, see: Calov *et al.* (1992); Dadachov *et al.* (2000); Tang *et al.* (2001).



## Experimental

## Crystal data

$(\text{C}_6\text{H}_{21}\text{N}_4)[\text{TiF}_6]\text{F}$   
 $M_r = 330.14$   
 Monoclinic,  $P2_1/c$   
 $a = 16.265$  (4) Å  
 $b = 8.089$  (3) Å  
 $c = 21.778$  (5) Å  
 $\beta = 110.54$  (2)°

$V = 2683.1$  (13) Å<sup>3</sup>  
 $Z = 8$   
 Mo  $K\alpha$  radiation  
 $\mu = 0.71$  mm<sup>-1</sup>  
 $T = 298$  (2) K  
 $0.18 \times 0.13 \times 0.06$  mm

## Data collection

Siemens AED2 diffractometer  
 Absorption correction: Gaussian  
 (SHELX76; Sheldrick, 2008)  
 $T_{\min} = 0.850$ ,  $T_{\max} = 0.929$   
 6191 measured reflections

6133 independent reflections  
 3531 reflections with  $I > 2\sigma(I)$   
 3 standard reflections  
 frequency: 120 min  
 intensity decay: 15%

## Refinement

$R[F^2 > 2\sigma(F^2)] = 0.061$   
 $wR(F^2) = 0.155$   
 $S = 1.12$   
 6133 reflections

332 parameters  
 H-atom parameters constrained  
 $\Delta\rho_{\max} = 1.37$  e Å<sup>-3</sup>  
 $\Delta\rho_{\min} = -0.42$  e Å<sup>-3</sup>

Table 1

Selected bond lengths (Å).

|        |           |         |           |
|--------|-----------|---------|-----------|
| Ti1—F1 | 1.796 (3) | Ti2—F8  | 1.803 (3) |
| Ti1—F2 | 1.826 (3) | Ti2—F7  | 1.821 (3) |
| Ti1—F4 | 1.856 (3) | Ti2—F9  | 1.825 (3) |
| Ti1—F5 | 1.865 (3) | Ti2—F10 | 1.827 (3) |
| Ti1—F3 | 1.868 (3) | Ti2—F11 | 1.832 (3) |
| Ti1—F6 | 1.882 (3) | Ti2—F12 | 1.856 (3) |

Table 2

Hydrogen-bond geometry (Å, °).

| $D-\text{H}\cdots A$              | $D-\text{H}$ | $\text{H}\cdots A$ | $D\cdots A$ | $D-\text{H}\cdots A$ |
|-----------------------------------|--------------|--------------------|-------------|----------------------|
| N2—H2C $\cdots$ F13               | 0.89         | 1.90               | 2.773 (5)   | 165                  |
| N2—H2D $\cdots$ F6 <sup>i</sup>   | 0.89         | 2.04               | 2.865 (5)   | 154                  |
| N2—H2E $\cdots$ F13 <sup>i</sup>  | 0.89         | 1.84               | 2.725 (5)   | 172                  |
| N3—H3C $\cdots$ F13               | 0.89         | 1.86               | 2.700 (5)   | 157                  |
| N3—H3C $\cdots$ N1                | 0.89         | 2.52               | 2.948 (6)   | 110                  |
| N3—H3D $\cdots$ F3                | 0.89         | 1.90               | 2.726 (5)   | 154                  |
| N3—H3E $\cdots$ F9                | 0.89         | 1.84               | 2.717 (5)   | 167                  |
| N4—H4C $\cdots$ F13               | 0.89         | 1.83               | 2.692 (5)   | 162                  |
| N4—H4D $\cdots$ F12 <sup>i</sup>  | 0.89         | 2.01               | 2.835 (5)   | 153                  |
| N4—H4E $\cdots$ F5                | 0.89         | 1.84               | 2.712 (5)   | 168                  |
| N6—H6C $\cdots$ F14               | 0.89         | 1.84               | 2.696 (5)   | 162                  |
| N6—H6D $\cdots$ F10 <sup>ii</sup> | 0.89         | 2.00               | 2.823 (5)   | 154                  |
| N6—H6E $\cdots$ F4 <sup>iii</sup> | 0.89         | 1.90               | 2.749 (5)   | 160                  |
| N7—H7C $\cdots$ F14               | 0.89         | 1.82               | 2.699 (5)   | 169                  |
| N7—H7D $\cdots$ F2 <sup>iii</sup> | 0.89         | 2.24               | 2.876 (5)   | 129                  |
| N7—H7E $\cdots$ F7 <sup>i</sup>   | 0.89         | 2.08               | 2.916 (5)   | 157                  |
| N7—H7E $\cdots$ F10 <sup>i</sup>  | 0.89         | 2.41               | 2.972 (5)   | 121                  |
| N8—H8C $\cdots$ F14               | 0.89         | 1.91               | 2.791 (5)   | 168                  |
| N8—H8D $\cdots$ F6                | 0.89         | 2.14               | 2.879 (5)   | 140                  |
| N8—H8E $\cdots$ F14 <sup>iv</sup> | 0.89         | 1.81               | 2.702 (5)   | 177                  |

Symmetry codes: (i)  $-x + 1, y - \frac{1}{2}, -z + \frac{3}{2}$ ; (ii)  $x - 1, y, z$ ; (iii)  $-x, y - \frac{1}{2}, -z + \frac{3}{2}$ ; (iv)  $-x, y + \frac{1}{2}, -z + \frac{3}{2}$ .

Data collection: *STADIA* (Stoe & Cie, 1998); cell refinement: *STADIA*; data reduction: *X-RED* (Stoe & Cie, 1998); program(s) used to solve structure: *SHELXS97* (Sheldrick, 2008); program(s) used to refine structure: *SHELXL97* (Sheldrick, 2008); molecular graphics: *DIAMOND* (Brandenburg, 2001); software used to prepare material for publication: *enCIFer* (Allen *et al.*, 2004).

Supplementary data and figures for this paper are available from the IUCr electronic archives (Reference: NC2095).

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**supplementary materials**

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## Diethylenetriaminium hexafluoridotitanate(IV) fluoride

J. Lhoste, K. Adil, M. Leblanc and V. Maisonneuve

### Comment

To date, only a few organic-inorganic fluorotitanates were reported. The first compound  $\{(\text{CN}_3\text{H}_6)[\text{TiF}_6]\}$ , described by Calov *et al.* (1992), is built up from  $(\text{TiF}_6)$  monomers and guanidinium cations. Dadachov *et al.* (2000) and Tang *et al.* (2001) reported the synthesis of piperazinium  $\{(\text{C}_4\text{N}_2\text{H}_{12})_2[\text{Ti}_2\text{F}_{10}]2(\text{H}_2\text{O})\}$  and piperidinium  $\{[\text{C}_5\text{H}_6\text{N}_2]2(\text{Ti}_2\text{F}_{11})(\text{H}_3\text{O})(\text{H}_2\text{O})\}$  fluorotitanates respectively, built up from  $(\text{Ti}_2\text{F}_{10})^{2-}$  or  $(\text{Ti}_2\text{F}_{11})^{3-}$  dimers. As a part of our ongoing investigations in this field (Adil *et al.*, 2006) we now report the synthesis and structure of the title compound, (I).

The asymmetric unit of (I) consists of two crystallographically independent  $(\text{TiF}_6)^{2-}$  anions, two fluoride anions and two triprotonated tris(2-aminoethyl)amine (tren) cations, all of them located in general positions (Fig. 1). The  $\text{TiF}_6$  anions form slightly distorted octahedra and the environment of both independent anions is different (Table 1). Both  $\text{TiF}_6$  anions are connected to the cations via  $\text{N}\cdots\text{H}\cdots\text{F}$  hydrogen bonding (Figure 2 and Table 2).

The two isolated fluoride anions are also hydrogen bonded to the  $[\text{H}_3\text{tren}]^{3+}$  cations with  $\text{N}\cdots\text{H}\cdots\text{F}$  distances ranging from 2.692 (5)Å to 2.791 (5)Å (Figure 2 and Table 2).

### Experimental

The synthesis was performed by using a microwave-assisted route. Crystals were prepared from a mixture of titanium(IV) oxide (79 mg, 1 mmol), tris(2-aminoethyl)amine (0.230 ml, 1.52 mmol), hydrogen fluoride (40%, 0.130 ml, 2.95 mmol) and ethanol (10 ml, 35 mmol). The mixture was transferred into a teflon autoclave installed in a CEM microwave oven at 493 K for 1 hour under a constant pressure of 22 bar. Finally, the solid product was washed with ethanol and dried in air at room temperature to yield colourless parallelepipeds of (I).

### Refinement

A number of mis-measured reflections were omitted from the refinement.

The hydrogen atoms were positioned with idealized geometry ( $\text{C}\text{---}\text{H} = 0.88\text{--}0.97\text{Å}$ ,  $\text{N}\text{---}\text{H} = 0.89\text{Å}$ ) and modelled as riding with a group  $U_{\text{iso}}$  value refined.

The highest difference is 2.49 Å from H4A. It might be that this peak corresponds to a small amount of water, which cannot be proven. Therefore, this electron density was not considered in the final refinement.

## Figures

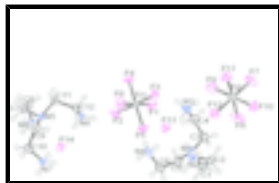


Fig. 1. Crystal structure of (I) with displacement ellipsoids for the non-hydrogen atoms drawn at the 50% probability level.

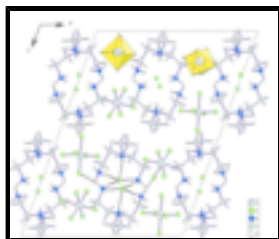


Fig. 2. Crystal packing of (I) with view along [010]. Hydrogen bonding is shown as dashed lines.

## Diethylenetriaminium hexafluoridotitanate(IV) fluoride

### Crystal data

(C<sub>6</sub>H<sub>21</sub>N<sub>4</sub>)[TiF<sub>6</sub>]F

$M_r = 330.14$

Monoclinic,  $P2_1/c$

Hall symbol: -P 2ybc

$a = 16.265 (4) \text{ \AA}$

$b = 8.089 (3) \text{ \AA}$

$c = 21.778 (5) \text{ \AA}$

$\beta = 110.54 (2)^\circ$

$V = 2683.1 (13) \text{ \AA}^3$

$Z = 8$

$F_{000} = 1360$

$D_x = 1.635 \text{ Mg m}^{-3}$

Mo  $K\alpha$  radiation

$\lambda = 0.71069 \text{ \AA}$

Cell parameters from 32 reflections

$\theta = 29.1\text{--}30.9^\circ$

$\mu = 0.71 \text{ mm}^{-1}$

$T = 298 (2) \text{ K}$

Parallelepiped, colourless

$0.18 \times 0.13 \times 0.06 \text{ mm}$

### Data collection

Siemens AED2  
diffractometer

Radiation source: fine-focus sealed tube

Monochromator: graphite

$T = 295(2) \text{ K}$

$2\theta/\omega$  scans

Absorption correction: Gaussian  
(SHELX76; Sheldrick, 2008)

$T_{\min} = 0.850$ ,  $T_{\max} = 0.929$

6191 measured reflections

6133 independent reflections

3531 reflections with  $I > 2\sigma(I)$

$R_{\text{int}} = 0.0000$

$\theta_{\max} = 27.5^\circ$

$\theta_{\min} = 2.0^\circ$

$h = -21 \rightarrow 19$

$k = 0 \rightarrow 10$

$l = 0 \rightarrow 28$

3 standard reflections

every 120 min

intensity decay: 15%

Refinement

|  |  |
|--|--|
| Refinement on $F^2$  | Secondary atom site location: difference Fourier map     |
| Least-squares matrix: full                                     | Hydrogen site location: inferred from neighbouring sites |
| $R[F^2 > 2\sigma(F^2)] = 0.061$                                | H-atom parameters constrained                            |
| $wR(F^2) = 0.155$  | $w = 1/[\sigma^2(F_o^2) + (0.0532P)^2 + 2.5558P]$        |
| $S = 1.12$   | where $P = (F_o^2 + 2F_c^2)/3$                           |
| 6133 reflections   | $(\Delta/\sigma)_{\max} = 0.001$                         |
| 332 parameters   | $\Delta\rho_{\max} = 1.37 \text{ e } \text{\AA}^{-3}$    |
| Primary atom site location: structure-invariant direct methods | $\Delta\rho_{\min} = -0.42 \text{ e } \text{\AA}^{-3}$   |
|  | Extinction correction: none                              |

Special details

**Geometry.** All e.s.d.'s (except the e.s.d. in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell e.s.d.'s are taken into account individually in the estimation of e.s.d.'s in distances, angles and torsion angles; correlations between e.s.d.'s in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell e.s.d.'s is used for estimating e.s.d.'s involving l.s. planes.

**Refinement.** Refinement of  $F^2$  against ALL reflections. The weighted  $R$ -factor  $wR$  and goodness of fit  $S$  are based on  $F^2$ , conventional  $R$ -factors  $R$  are based on  $F$ , with  $F$  set to zero for negative  $F^2$ . The threshold expression of  $F^2 > \sigma(F^2)$  is used only for calculating  $R$ -factors(gt) *etc.* and is not relevant to the choice of reflections for refinement.  $R$ -factors based on  $F^2$  are statistically about twice as large as those based on  $F$ , and  $R$ -factors based on ALL data will be even larger.

Fractional atomic coordinates and isotropic or equivalent isotropic displacement parameters ( $\text{\AA}^2$ )

|     | $x$          | $y$          | $z$          | $U_{\text{iso}}^*/U_{\text{eq}}$ |
|-----|--------------|--------------|--------------|----------------------------------|
| Ti1 | 0.18135 (5)  | 0.59284 (10) | 0.60307 (4)  | 0.02406 (18)                     |
| Ti2 | 0.70766 (5)  | 0.58675 (11) | 0.64839 (4)  | 0.0319 (2)                       |
| F1  | 0.1489 (3)   | 0.5816 (4)   | 0.51539 (14) | 0.0687 (10)                      |
| F2  | 0.07464 (18) | 0.5254 (4)   | 0.60403 (17) | 0.0582 (9)                       |
| F3  | 0.29513 (18) | 0.6604 (4)   | 0.61299 (17) | 0.0539 (8)                       |
| F4  | 0.14665 (19) | 0.8126 (3)   | 0.59720 (15) | 0.0469 (7)                       |
| F5  | 0.2192 (2)   | 0.3737 (3)   | 0.61004 (16) | 0.0492 (8)                       |
| F6  | 0.2182 (2)   | 0.6079 (5)   | 0.69502 (13) | 0.0557 (9)                       |
| F7  | 0.72742 (19) | 0.7113 (4)   | 0.58528 (14) | 0.0518 (8)                       |
| F8  | 0.6614 (2)   | 0.4174 (4)   | 0.59328 (14) | 0.0631 (10)                      |
| F9  | 0.5986 (2)   | 0.6765 (4)   | 0.6291 (2)   | 0.0817 (13)                      |
| F10 | 0.81774 (18) | 0.4997 (4)   | 0.66930 (15) | 0.0494 (8)                       |
| F11 | 0.7527 (2)   | 0.7485 (4)   | 0.70991 (15) | 0.0533 (8)                       |
| F12 | 0.6933 (2)   | 0.4627 (4)   | 0.71561 (15) | 0.0555 (9)                       |
| N1  | 0.4459 (2)   | 0.1509 (5)   | 0.60450 (17) | 0.0276 (8)                       |
| C1  | 0.5134 (3)   | 0.0224 (6)   | 0.6192 (2)   | 0.0361 (11)                      |
| H1A | 0.5186       | -0.0159      | 0.5785       | 0.044 (2)*                       |
| H1B | 0.4952       | -0.0708      | 0.6394       | 0.044 (2)*                       |

## supplementary materials

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|      |             |            |              |             |
|------|-------------|------------|--------------|-------------|
| C2   | 0.6020 (3)  | 0.0814 (6) | 0.6642 (2)   | 0.0342 (10) |
| H2A  | 0.6448      | -0.0063    | 0.6703       | 0.044 (2)*  |
| H2B  | 0.6206      | 0.1748     | 0.6444       | 0.044 (2)*  |
| N2   | 0.5983 (2)  | 0.1311 (5) | 0.72899 (18) | 0.0333 (9)  |
| H2C  | 0.5635      | 0.2188     | 0.7239       | 0.044 (2)*  |
| H2D  | 0.6521      | 0.1565     | 0.7560       | 0.044 (2)*  |
| H2E  | 0.5773      | 0.0479     | 0.7458       | 0.044 (2)*  |
| C3   | 0.4511 (3)  | 0.2578 (6) | 0.5509 (2)   | 0.0392 (12) |
| H3A  | 0.4246      | 0.2012     | 0.5093       | 0.044 (2)*  |
| H3B  | 0.5123      | 0.2784     | 0.5571       | 0.044 (2)*  |
| C4   | 0.4048 (3)  | 0.4209 (7) | 0.5489 (2)   | 0.0418 (12) |
| H4A  | 0.4078      | 0.4863     | 0.5124       | 0.044 (2)*  |
| H4B  | 0.3434      | 0.4006     | 0.5419       | 0.044 (2)*  |
| N3   | 0.4453 (3)  | 0.5149 (5) | 0.61097 (19) | 0.0379 (9)  |
| H3C  | 0.4595      | 0.4455     | 0.6448       | 0.044 (2)*  |
| H3D  | 0.4073      | 0.5894     | 0.6150       | 0.044 (2)*  |
| H3E  | 0.4935      | 0.5660     | 0.6103       | 0.044 (2)*  |
| C5   | 0.3582 (3)  | 0.0778 (7) | 0.5890 (2)   | 0.0394 (11) |
| H5A  | 0.3532      | -0.0187    | 0.5615       | 0.044 (2)*  |
| H5B  | 0.3142      | 0.1572     | 0.5645       | 0.044 (2)*  |
| C6   | 0.3406 (3)  | 0.0281 (6) | 0.6498 (3)   | 0.0399 (12) |
| H6A  | 0.2837      | -0.0253    | 0.6373       | 0.044 (2)*  |
| H6B  | 0.3847      | -0.0512    | 0.6743       | 0.044 (2)*  |
| N4   | 0.3420 (2)  | 0.1714 (5) | 0.69203 (18) | 0.0375 (10) |
| H4C  | 0.3941      | 0.2208     | 0.7036       | 0.044 (2)*  |
| H4D  | 0.3325      | 0.1373     | 0.7278       | 0.044 (2)*  |
| H4E  | 0.3002      | 0.2425     | 0.6702       | 0.044 (2)*  |
| N5   | 0.0735 (2)  | 0.5437 (4) | 0.89540 (17) | 0.0257 (8)  |
| C7   | -0.0032 (3) | 0.6180 (6) | 0.9046 (2)   | 0.0303 (10) |
| H7A  | 0.0129      | 0.7239     | 0.9263       | 0.044 (2)*  |
| H7B  | -0.0232     | 0.5471     | 0.9324       | 0.044 (2)*  |
| C8   | -0.0768 (3) | 0.6422 (6) | 0.8393 (2)   | 0.0371 (11) |
| H8A  | -0.1257     | 0.6977     | 0.8462       | 0.044 (2)*  |
| H8B  | -0.0566     | 0.7112     | 0.8111       | 0.044 (2)*  |
| N6   | -0.1063 (2) | 0.4800 (5) | 0.80724 (18) | 0.0396 (10) |
| H6C  | -0.0602     | 0.4245     | 0.8049       | 0.044 (2)*  |
| H6D  | -0.1447     | 0.4962     | 0.7670       | 0.044 (2)*  |
| H6E  | -0.1316     | 0.4222     | 0.8305       | 0.044 (2)*  |
| C9   | 0.1286 (3)  | 0.4546 (6) | 0.9547 (2)   | 0.0330 (10) |
| H9A  | 0.1348      | 0.5216     | 0.9930       | 0.044 (2)*  |
| H9B  | 0.1867      | 0.4386     | 0.9526       | 0.044 (2)*  |
| C10  | 0.0905 (3)  | 0.2884 (6) | 0.9620 (2)   | 0.0324 (10) |
| H10A | 0.1238      | 0.2425     | 1.0047       | 0.044 (2)*  |
| H10B | 0.0304      | 0.3030     | 0.9598       | 0.044 (2)*  |
| N7   | 0.0924 (3)  | 0.1710 (5) | 0.91024 (19) | 0.0350 (9)  |
| H7C  | 0.0633      | 0.2141     | 0.8710       | 0.044 (2)*  |
| H7D  | 0.0673      | 0.0763     | 0.9148       | 0.044 (2)*  |
| H7E  | 0.1478      | 0.1522     | 0.9138       | 0.044 (2)*  |
| C11  | 0.1253 (3)  | 0.6685 (5) | 0.8757 (2)   | 0.0309 (10) |

|      |              |            |              |             |
|------|--------------|------------|--------------|-------------|
| H11A | 0.1671       | 0.7186     | 0.9147       | 0.044 (2)*  |
| H11B | 0.0864       | 0.7548     | 0.8508       | 0.044 (2)*  |
| C12  | 0.1743 (3)   | 0.5946 (6) | 0.8347 (2)   | 0.0319 (10) |
| H12A | 0.2105       | 0.6789     | 0.8252       | 0.044 (2)*  |
| H12B | 0.2126       | 0.5069     | 0.8592       | 0.044 (2)*  |
| N8   | 0.1116 (2)   | 0.5266 (5) | 0.77194 (18) | 0.0329 (9)  |
| H8C  | 0.0850       | 0.4378     | 0.7804       | 0.044 (2)*  |
| H8D  | 0.1408       | 0.4986     | 0.7458       | 0.044 (2)*  |
| H8E  | 0.0716       | 0.6030     | 0.7523       | 0.044 (2)*  |
| F13  | 0.48067 (17) | 0.3777 (3) | 0.73054 (12) | 0.0381 (6)  |
| F14  | 0.00692 (17) | 0.2652 (3) | 0.78508 (13) | 0.0362 (6)  |

*Atomic displacement parameters ( $\text{\AA}^2$ )*

|     | $U^{11}$    | $U^{22}$    | $U^{33}$    | $U^{12}$     | $U^{13}$     | $U^{23}$     |
|-----|-------------|-------------|-------------|--------------|--------------|--------------|
| Ti1 | 0.0232 (4)  | 0.0229 (4)  | 0.0258 (4)  | 0.0008 (3)   | 0.0081 (3)   | -0.0022 (3)  |
| Ti2 | 0.0313 (4)  | 0.0306 (4)  | 0.0335 (4)  | 0.0001 (4)   | 0.0109 (3)   | 0.0052 (4)   |
| F1  | 0.116 (3)   | 0.052 (2)   | 0.0285 (15) | 0.000 (2)    | 0.0141 (17)  | -0.0044 (16) |
| F2  | 0.0296 (15) | 0.0481 (19) | 0.096 (3)   | -0.0058 (14) | 0.0206 (16)  | 0.0027 (18)  |
| F3  | 0.0365 (16) | 0.0480 (18) | 0.088 (2)   | -0.0072 (14) | 0.0353 (17)  | -0.0135 (17) |
| F4  | 0.0507 (18) | 0.0262 (15) | 0.064 (2)   | 0.0073 (13)  | 0.0211 (15)  | -0.0005 (14) |
| F5  | 0.0505 (17) | 0.0293 (16) | 0.066 (2)   | 0.0112 (13)  | 0.0185 (15)  | 0.0061 (14)  |
| F6  | 0.0519 (18) | 0.086 (2)   | 0.0284 (15) | -0.0037 (18) | 0.0125 (13)  | -0.0022 (16) |
| F7  | 0.0519 (18) | 0.0520 (19) | 0.0443 (17) | -0.0129 (15) | 0.0079 (14)  | 0.0156 (15)  |
| F8  | 0.088 (2)   | 0.055 (2)   | 0.0351 (16) | -0.0295 (19) | 0.0079 (16)  | 0.0026 (16)  |
| F9  | 0.0399 (19) | 0.046 (2)   | 0.163 (4)   | 0.0094 (16)  | 0.041 (2)    | 0.025 (2)    |
| F10 | 0.0447 (17) | 0.0482 (19) | 0.0568 (18) | 0.0151 (15)  | 0.0196 (15)  | 0.0040 (16)  |
| F11 | 0.071 (2)   | 0.0408 (17) | 0.0527 (19) | -0.0096 (16) | 0.0270 (17)  | -0.0140 (15) |
| F12 | 0.094 (2)   | 0.0410 (17) | 0.0477 (18) | -0.0066 (17) | 0.0445 (18)  | 0.0021 (14)  |
| N1  | 0.0255 (18) | 0.0327 (19) | 0.0250 (18) | 0.0021 (15)  | 0.0096 (15)  | -0.0017 (16) |
| C1  | 0.041 (3)   | 0.031 (2)   | 0.037 (3)   | 0.009 (2)    | 0.015 (2)    | -0.002 (2)   |
| C2  | 0.028 (2)   | 0.033 (2)   | 0.043 (3)   | 0.010 (2)    | 0.015 (2)    | 0.007 (2)    |
| N2  | 0.0265 (19) | 0.032 (2)   | 0.035 (2)   | -0.0022 (16) | 0.0028 (16)  | 0.0040 (17)  |
| C3  | 0.044 (3)   | 0.052 (3)   | 0.023 (2)   | 0.007 (2)    | 0.014 (2)    | 0.003 (2)    |
| C4  | 0.042 (3)   | 0.050 (3)   | 0.029 (2)   | 0.008 (3)    | 0.008 (2)    | 0.013 (2)    |
| N3  | 0.034 (2)   | 0.034 (2)   | 0.044 (2)   | 0.0034 (18)  | 0.0114 (19)  | 0.0111 (19)  |
| C5  | 0.031 (2)   | 0.044 (3)   | 0.037 (3)   | -0.005 (2)   | 0.004 (2)    | -0.014 (2)   |
| C6  | 0.033 (2)   | 0.031 (2)   | 0.055 (3)   | -0.008 (2)   | 0.015 (2)    | 0.004 (2)    |
| N4  | 0.029 (2)   | 0.052 (3)   | 0.033 (2)   | -0.0063 (19) | 0.0137 (17)  | 0.0057 (19)  |
| N5  | 0.0284 (18) | 0.0223 (18) | 0.0283 (18) | -0.0008 (14) | 0.0121 (15)  | 0.0013 (14)  |
| C7  | 0.032 (2)   | 0.030 (2)   | 0.035 (2)   | 0.0019 (19)  | 0.0192 (19)  | -0.0014 (19) |
| C8  | 0.036 (3)   | 0.037 (3)   | 0.042 (3)   | 0.014 (2)    | 0.018 (2)    | 0.013 (2)    |
| N6  | 0.032 (2)   | 0.053 (3)   | 0.031 (2)   | 0.0091 (19)  | 0.0073 (17)  | 0.003 (2)    |
| C9  | 0.030 (2)   | 0.036 (3)   | 0.025 (2)   | 0.0015 (19)  | -0.0001 (18) | -0.0033 (19) |
| C10 | 0.042 (3)   | 0.030 (2)   | 0.024 (2)   | 0.006 (2)    | 0.010 (2)    | 0.0087 (19)  |
| N7  | 0.045 (2)   | 0.026 (2)   | 0.038 (2)   | 0.0029 (18)  | 0.0197 (19)  | 0.0046 (17)  |
| C11 | 0.036 (2)   | 0.023 (2)   | 0.038 (3)   | -0.0053 (19) | 0.019 (2)    | -0.0027 (19) |
| C12 | 0.025 (2)   | 0.031 (2)   | 0.044 (3)   | -0.003 (2)   | 0.0176 (19)  | 0.000 (2)    |

## supplementary materials

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|     |             |             |             |              |             |              |
|-----|-------------|-------------|-------------|--------------|-------------|--------------|
| N8  | 0.039 (2)   | 0.030 (2)   | 0.038 (2)   | 0.0009 (17)  | 0.0249 (18) | 0.0004 (17)  |
| F13 | 0.0377 (15) | 0.0401 (16) | 0.0357 (15) | -0.0005 (12) | 0.0119 (12) | -0.0088 (12) |
| F14 | 0.0398 (15) | 0.0338 (15) | 0.0352 (14) | -0.0026 (12) | 0.0134 (12) | -0.0064 (12) |

### *Geometric parameters (Å, °)*

|           |             |            |           |
|-----------|-------------|------------|-----------|
| Ti1—F1    | 1.796 (3)   | C6—N4      | 1.475 (6) |
| Ti1—F2    | 1.826 (3)   | C6—H6A     | 0.9700    |
| Ti1—F4    | 1.856 (3)   | C6—H6B     | 0.9700    |
| Ti1—F5    | 1.865 (3)   | N4—H4C     | 0.8900    |
| Ti1—F3    | 1.868 (3)   | N4—H4D     | 0.8900    |
| Ti1—F6    | 1.882 (3)   | N4—H4E     | 0.8900    |
| Ti2—F8    | 1.803 (3)   | N5—C7      | 1.459 (5) |
| Ti2—F7    | 1.821 (3)   | N5—C11     | 1.472 (5) |
| Ti2—F9    | 1.825 (3)   | N5—C9      | 1.475 (5) |
| Ti2—F10   | 1.827 (3)   | C7—C8      | 1.516 (6) |
| Ti2—F11   | 1.832 (3)   | C7—H7A     | 0.9700    |
| Ti2—F12   | 1.856 (3)   | C7—H7B     | 0.9700    |
| N1—C1     | 1.463 (6)   | C8—N6      | 1.484 (6) |
| N1—C5     | 1.470 (6)   | C8—H8A     | 0.9700    |
| N1—C3     | 1.479 (6)   | C8—H8B     | 0.9700    |
| C1—C2     | 1.507 (6)   | N6—H6C     | 0.8900    |
| C1—H1A    | 0.9700      | N6—H6D     | 0.8900    |
| C1—H1B    | 0.9700      | N6—H6E     | 0.8900    |
| C2—N2     | 1.487 (6)   | C9—C10     | 1.512 (6) |
| C2—H2A    | 0.9700      | C9—H9A     | 0.9700    |
| C2—H2B    | 0.9700      | C9—H9B     | 0.9700    |
| N2—H2C    | 0.8900      | C10—N7     | 1.483 (6) |
| N2—H2D    | 0.8900      | C10—H10A   | 0.9700    |
| N2—H2E    | 0.8900      | C10—H10B   | 0.9700    |
| C3—C4     | 1.512 (7)   | N7—H7C     | 0.8900    |
| C3—H3A    | 0.9700      | N7—H7D     | 0.8900    |
| C3—H3B    | 0.9700      | N7—H7E     | 0.8900    |
| C4—N3     | 1.489 (6)   | C11—C12    | 1.513 (6) |
| C4—H4A    | 0.9700      | C11—H11A   | 0.9700    |
| C4—H4B    | 0.9700      | C11—H11B   | 0.9700    |
| N3—H3C    | 0.8900      | C12—N8     | 1.494 (6) |
| N3—H3D    | 0.8900      | C12—H12A   | 0.9700    |
| N3—H3E    | 0.8900      | C12—H12B   | 0.9700    |
| C5—C6     | 1.504 (7)   | N8—H8C     | 0.8900    |
| C5—H5A    | 0.9700      | N8—H8D     | 0.8900    |
| C5—H5B    | 0.9700      | N8—H8E     | 0.8900    |
| F1—Ti1—F2 | 94.09 (17)  | N1—C5—H5B  | 109.2     |
| F1—Ti1—F4 | 90.38 (15)  | C6—C5—H5B  | 109.2     |
| F2—Ti1—F4 | 91.12 (14)  | H5A—C5—H5B | 107.9     |
| F1—Ti1—F5 | 90.21 (15)  | N4—C6—C5   | 111.9 (4) |
| F2—Ti1—F5 | 90.17 (14)  | N4—C6—H6A  | 109.2     |
| F4—Ti1—F5 | 178.55 (14) | C5—C6—H6A  | 109.2     |
| F1—Ti1—F3 | 92.71 (17)  | N4—C6—H6B  | 109.2     |



|             |             |               |           |
|-------------|-------------|---------------|-----------|
| F2—Ti1—F3   | 173.16 (16) | C5—C6—H6B     | 109.2     |
| F4—Ti1—F3   | 89.59 (14)  | H6A—C6—H6B    | 107.9     |
| F5—Ti1—F3   | 89.06 (14)  | C6—N4—H4C     | 109.5     |
| F1—Ti1—F6   | 178.38 (17) | C6—N4—H4D     | 109.5     |
| F2—Ti1—F6   | 87.50 (15)  | H4C—N4—H4D    | 109.5     |
| F4—Ti1—F6   | 89.26 (15)  | C6—N4—H4E     | 109.5     |
| F5—Ti1—F6   | 90.11 (15)  | H4C—N4—H4E    | 109.5     |
| F3—Ti1—F6   | 85.71 (15)  | H4D—N4—H4E    | 109.5     |
| F8—Ti2—F7   | 93.49 (14)  | C7—N5—C11     | 111.2 (3) |
| F8—Ti2—F9   | 90.23 (18)  | C7—N5—C9      | 111.6 (3) |
| F7—Ti2—F9   | 91.21 (16)  | C11—N5—C9     | 110.8 (3) |
| F8—Ti2—F10  | 90.95 (16)  | N5—C7—C8      | 110.9 (4) |
| F7—Ti2—F10  | 89.10 (15)  | N5—C7—H7A     | 109.5     |
| F9—Ti2—F10  | 178.75 (19) | C8—C7—H7A     | 109.5     |
| F8—Ti2—F11  | 175.05 (15) | N5—C7—H7B     | 109.5     |
| F7—Ti2—F11  | 91.46 (15)  | C8—C7—H7B     | 109.5     |
| F9—Ti2—F11  | 89.50 (18)  | H7A—C7—H7B    | 108.0     |
| F10—Ti2—F11 | 89.29 (15)  | N6—C8—C7      | 110.2 (4) |
| F8—Ti2—F12  | 88.59 (14)  | N6—C8—H8A     | 109.6     |
| F7—Ti2—F12  | 177.05 (15) | C7—C8—H8A     | 109.6     |
| F9—Ti2—F12  | 90.86 (17)  | N6—C8—H8B     | 109.6     |
| F10—Ti2—F12 | 88.78 (15)  | C7—C8—H8B     | 109.6     |
| F11—Ti2—F12 | 86.47 (14)  | H8A—C8—H8B    | 108.1     |
| C1—N1—C5    | 111.0 (4)   | C8—N6—H6C     | 109.5     |
| C1—N1—C3    | 110.0 (4)   | C8—N6—H6D     | 109.5     |
| C5—N1—C3    | 111.9 (4)   | H6C—N6—H6D    | 109.5     |
| N1—C1—C2    | 112.9 (4)   | C8—N6—H6E     | 109.5     |
| N1—C1—H1A   | 109.0       | H6C—N6—H6E    | 109.5     |
| C2—C1—H1A   | 109.0       | H6D—N6—H6E    | 109.5     |
| N1—C1—H1B   | 109.0       | N5—C9—C10     | 112.4 (3) |
| C2—C1—H1B   | 109.0       | N5—C9—H9A     | 109.1     |
| H1A—C1—H1B  | 107.8       | C10—C9—H9A    | 109.1     |
| N2—C2—C1    | 110.8 (4)   | N5—C9—H9B     | 109.1     |
| N2—C2—H2A   | 109.5       | C10—C9—H9B    | 109.1     |
| C1—C2—H2A   | 109.5       | H9A—C9—H9B    | 107.9     |
| N2—C2—H2B   | 109.5       | N7—C10—C9     | 111.7 (4) |
| C1—C2—H2B   | 109.5       | N7—C10—H10A   | 109.3     |
| H2A—C2—H2B  | 108.1       | C9—C10—H10A   | 109.3     |
| C2—N2—H2C   | 109.5       | N7—C10—H10B   | 109.3     |
| C2—N2—H2D   | 109.5       | C9—C10—H10B   | 109.3     |
| H2C—N2—H2D  | 109.5       | H10A—C10—H10B | 107.9     |
| C2—N2—H2E   | 109.5       | C10—N7—H7C    | 109.5     |
| H2C—N2—H2E  | 109.5       | C10—N7—H7D    | 109.5     |
| H2D—N2—H2E  | 109.5       | H7C—N7—H7D    | 109.5     |
| N1—C3—C4    | 111.6 (4)   | C10—N7—H7E    | 109.5     |
| N1—C3—H3A   | 109.3       | H7C—N7—H7E    | 109.5     |
| C4—C3—H3A   | 109.3       | H7D—N7—H7E    | 109.5     |
| N1—C3—H3B   | 109.3       | N5—C11—C12    | 112.0 (4) |
| C4—C3—H3B   | 109.3       | N5—C11—H11A   | 109.2     |

## supplementary materials

|            |           |               |           |
|------------|-----------|---------------|-----------|
| H3A—C3—H3B | 108.0     | C12—C11—H11A  | 109.2     |
| N3—C4—C3   | 111.2 (4) | N5—C11—H11B   | 109.2     |
| N3—C4—H4A  | 109.4     | C12—C11—H11B  | 109.2     |
| C3—C4—H4A  | 109.4     | H11A—C11—H11B | 107.9     |
| N3—C4—H4B  | 109.4     | N8—C12—C11    | 110.7 (3) |
| C3—C4—H4B  | 109.4     | N8—C12—H12A   | 109.5     |
| H4A—C4—H4B | 108.0     | C11—C12—H12A  | 109.5     |
| C4—N3—H3C  | 109.5     | N8—C12—H12B   | 109.5     |
| C4—N3—H3D  | 109.5     | C11—C12—H12B  | 109.5     |
| H3C—N3—H3D | 109.5     | H12A—C12—H12B | 108.1     |
| C4—N3—H3E  | 109.5     | C12—N8—H8C    | 109.5     |
| H3C—N3—H3E | 109.5     | C12—N8—H8D    | 109.5     |
| H3D—N3—H3E | 109.5     | H8C—N8—H8D    | 109.5     |
| N1—C5—C6   | 112.0 (4) | C12—N8—H8E    | 109.5     |
| N1—C5—H5A  | 109.2     | H8C—N8—H8E    | 109.5     |
| C6—C5—H5A  | 109.2     | H8D—N8—H8E    | 109.5     |

### Hydrogen-bond geometry ( $\text{\AA}$ , $^\circ$ )

| <i>D</i> —H $\cdots$ <i>A</i>     | <i>D</i> —H | H $\cdots$ <i>A</i> | <i>D</i> $\cdots$ <i>A</i> | <i>D</i> —H $\cdots$ <i>A</i> |
|-----------------------------------|-------------|---------------------|----------------------------|-------------------------------|
| N2—H2C $\cdots$ F13               | 0.89        | 1.90                | 2.773 (5)                  | 165                           |
| N2—H2D $\cdots$ F6 <sup>i</sup>   | 0.89        | 2.04                | 2.865 (5)                  | 154                           |
| N2—H2E $\cdots$ F13 <sup>i</sup>  | 0.89        | 1.84                | 2.725 (5)                  | 172                           |
| N3—H3C $\cdots$ F13               | 0.89        | 1.86                | 2.700 (5)                  | 157                           |
| N3—H3C $\cdots$ N1                | 0.89        | 2.52                | 2.948 (6)                  | 110                           |
| N3—H3D $\cdots$ F3                | 0.89        | 1.90                | 2.726 (5)                  | 154                           |
| N3—H3E $\cdots$ F9                | 0.89        | 1.84                | 2.717 (5)                  | 167                           |
| N4—H4C $\cdots$ F13               | 0.89        | 1.83                | 2.692 (5)                  | 162                           |
| N4—H4D $\cdots$ F12 <sup>i</sup>  | 0.89        | 2.01                | 2.835 (5)                  | 153                           |
| N4—H4E $\cdots$ F5                | 0.89        | 1.84                | 2.712 (5)                  | 168                           |
| N6—H6C $\cdots$ F14               | 0.89        | 1.84                | 2.696 (5)                  | 162                           |
| N6—H6D $\cdots$ F10 <sup>ii</sup> | 0.89        | 2.00                | 2.823 (5)                  | 154                           |
| N6—H6E $\cdots$ F4 <sup>iii</sup> | 0.89        | 1.90                | 2.749 (5)                  | 160                           |
| N7—H7C $\cdots$ F14               | 0.89        | 1.82                | 2.699 (5)                  | 169                           |
| N7—H7D $\cdots$ F2 <sup>iii</sup> | 0.89        | 2.24                | 2.876 (5)                  | 129                           |
| N7—H7E $\cdots$ F7 <sup>i</sup>   | 0.89        | 2.08                | 2.916 (5)                  | 157                           |
| N7—H7E $\cdots$ F10 <sup>i</sup>  | 0.89        | 2.41                | 2.972 (5)                  | 121                           |
| N8—H8C $\cdots$ F14               | 0.89        | 1.91                | 2.791 (5)                  | 168                           |
| N8—H8D $\cdots$ F6                | 0.89        | 2.14                | 2.879 (5)                  | 140                           |
| N8—H8E $\cdots$ F14 <sup>iv</sup> | 0.89        | 1.81                | 2.702 (5)                  | 177                           |

Symmetry codes: (i)  $-x+1, y-1/2, -z+3/2$ ; (ii)  $x-1, y, z$ ; (iii)  $-x, y-1/2, -z+3/2$ ; (iv)  $-x, y+1/2, -z+3/2$ .

Fig. 1

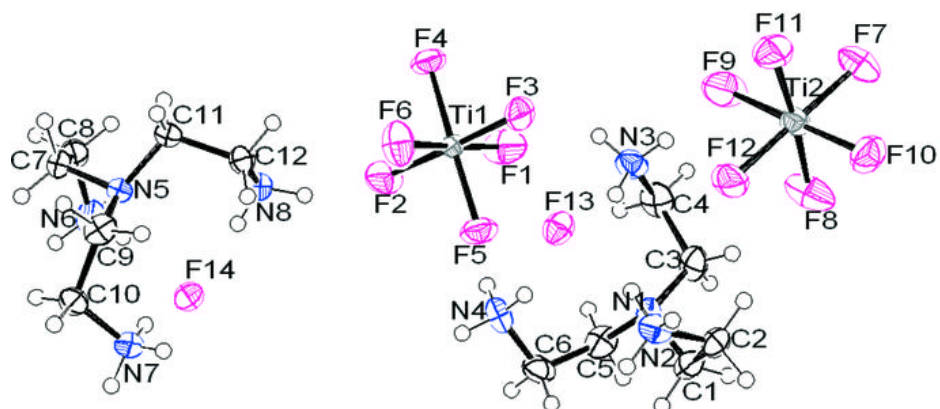


Fig. 2

